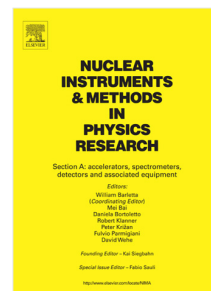


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## Operational properties of fine powder aerosol as radiation detection medium in gaseous proportional counters

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### Abstract

Due to its exceptional properties,  $^3\text{He}$  proportional counters are the golden standard for neutron detection, particularly in homeland security applications where large area detectors are deployed. However, in recent years  $^3\text{He}$  has become severely scarce, which led to a tremendous price increase and acquisition restrictions of this material. Motivated by this, the development of  $^3\text{He}$ -free solutions became a priority. In a previous work, we have established a novel concept for neutron detection: a proportional counter with boron carbide ( $\text{B}_4\text{C}$ ) fine powder suspended in the proportional gas forming a neutron sensitive aerosol that relies on the  $^{10}\text{B}$  neutron capture reaction. Computer simulations and prototype exposure to a cold neutron beam yielded favorable results, validating the detection concept, which may also be applied to hard x-ray and gamma ray detection by using fine particles made of a heavy element, such as Bi or Au. In this work we study the effect of the presence of  $\text{B}_4\text{C}$  microparticles in the charge gain and energy resolution of a proportional counter filled with Ar- $\text{CH}_4$  (90%-10%), by irradiation with x-rays from a  $^{55}\text{Fe}$  source. For the same applied voltage, an average gain loss by a factor of 36% and energy resolution (FWHM) increase by 15% (absolute value) was observed with the inclusion of  $\text{B}_4\text{C}$  microparticles. Intrinsic energy resolution was calculated, obtaining 15% for pure  $^{10}\text{B}$  operation and 32% in the presence of the microparticles. While the gain drop is recoverable by increasing anode voltage, energy resolution degradation may be a drawback in low energy applications, where energy resolution is favored over detection efficiency.

**Keywords:** Proportional counter, Neutron detection, Gamma ray detection,  $^{10}\text{B}$ ,  $^3\text{He}$  alternative.

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## 1. Introduction

### 1.1. The $^3\text{He}$ shortage crises

Neutron detectors are used in a wide range of applications, with the main consumers being homeland security instruments, such as Radiation Portal Monitors (RPMs) and handheld or backpack radiation monitoring systems. The  $^3\text{He}$  gaseous proportional counter is the most common neutron detector deployed, due to its excellent detection efficiency, good gamma-ray discrimination, non-toxicity and the fact that it can be used to produce large area detectors. However,  $^3\text{He}$  reserves are in decline which, in association with the great number of RPMs deployed, has led to an unsustainable situation, with the current demand for  $^3\text{He}$  surpassing its worldwide supply [1-8].

Since the scientific community became aware of the  $^3\text{He}$  shortage crises, research and development on  $^3\text{He}$ -free neutron detection solutions became a priority and innovative alternatives are being developed. A variety of techniques have been reported, including boron-lined detectors coupled to multi-wire proportional counters (MWPC) [9,10] and to gas electron multipliers (GEM) [11,12], arrays of boron-coated straws [13-15], aerogel and saturated foam detectors [16-18], scintillators [19,20], suspended lithium foils coupled to MWPC [21-23] and lithium backfilled microstructures [24,25].

This research is heavily restricted by the fact that only a few isotopes have the ability of absorbing neutrons and inducing nuclear capture reactions. In addition, for detection applications, the products of these reactions should comprise exclusively heavy charged particles, rather than gamma-rays or beta radiation. Based on these considerations, the list of alternative isotopes that can be used in neutron detection is narrowed to  $^6\text{Li}$  and  $^{10}\text{B}$ . Among these,  $^{10}\text{B}$  has a higher thermal neutron cross-section (3840 barn, versus 940 barn), which implies a greater detection efficiency potential.

### 1.2. $\text{B}_4\text{C}$ fine powder aerosol: a novel approach

A novel concept for neutron detection has been proposed in a previous work, which consists on a proportional counter filled with P10 ( $\text{Ar-CH}_4$ , 90%-10%) in which a boron-based fine powder is dispersed (boron-carbide was used), forming a neutron sensitive aerosol [26]. A detection efficiency of 4% was reported while irradiating a prototype with cold neutrons (5 Å). The boron-carbide ( $\text{B}_4\text{C}$ ) fine powder is made of natural boron, of which the  $^{10}\text{B}$  fraction is approximately 20%. Commercially available  $^{10}\text{B}$  enriched boron-carbide fine powder would lead to a 5-fold increase in detection efficiency.

In this neutron sensitive aerosol detection technique, the  $\text{B}_4\text{C}$  particles are suspended in the proportional gas by an appropriate gas flow which counter-acts the gravity force. As an incoming neutron interacts with the  $^{10}\text{B}$  atoms of the microparticles, 2 products are released in opposite directions: a  $^7\text{Li}$  ion (0.84 MeV) and an  $\alpha$ -particle (1.47 MeV). The main benefit of this detection concept is that both reaction products can escape the  $\text{B}_4\text{C}$  particles, since their range in this material is greater than the particles size. This allows for the deposition of a large fraction of the energy released by the neutron capture reaction in the filling gas, resulting in a full energy deposition peak (2.3 MeV) in the pulse height distribution of the detector. This feature is not possible to achieve with alternatives based on boron coating, in which the neutron capture occurs in a solid layer deposited on the walls of the detector. In these alternatives, for each reaction product that reaches the gas volume, the other one is inevitably lost to the detector walls, due to their ejection into opposite directions [27,28]. This leads to a two-step plateau in the pulse height distribution which extends to the low energy region (wall-effect)

46 and reduces the ability to discriminate between neutron captures and gamma-rays induced  
47 events.

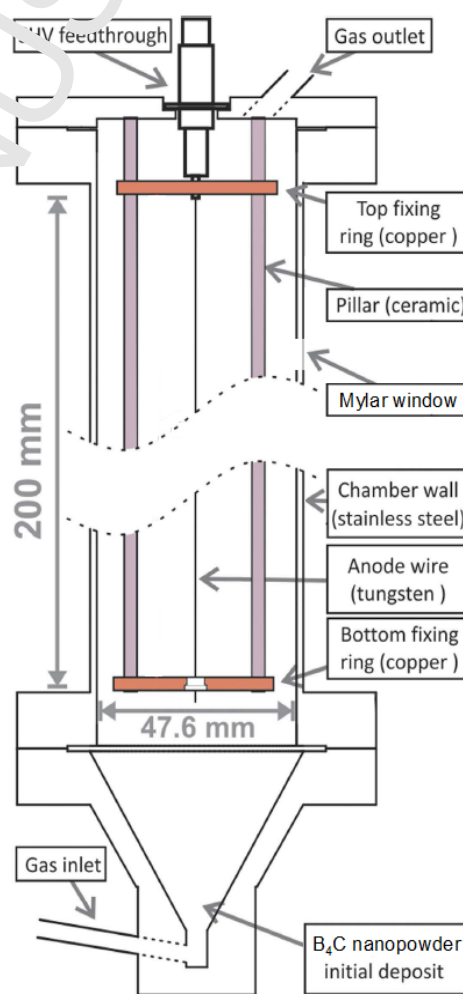
48 The presence of the  $B_4C$  fine powder in the proportional counter caused no operational  
49 issues, such as electrical discharges or a drastic gain decrease that prevented its operation.  
50 Nonetheless, it is essential to understand how the detector is affected by the presence of the  
51 fine powder in order to delineate an effective strategy for prototype optimization. The impact  
52 of the presence of  $B_4C$  particles in the gas gain and energy resolution of the proportional  
53 counter are assessed in this work. Tests were performed by irradiating the proportional  
54 counter, filled with an aerosol composed by  $B_4C$  microparticles dispersed in a P10  
55 atmosphere, by soft x-rays (5.9 keV) from a  $^{55}Fe$  source.

## 56 2. Methods

57 A scheme of the proportional counter used in this work is presented in Fig. 1. It consists of  
58 a stainless-steel cylinder with an inner diameter of 47.6 mm and a 50  $\mu m$  diameter tungsten  
59 anode wire stretched along its axis. The anode is electrically insulated from the walls (at ground  
60 potential) by ceramic feedthroughs. When a positive voltage is applied to the anode, an electric field is  
61 established inside the proportional counter reaching values above the threshold for charge multiplication in  
62 a small region around the anode wire. The proportional counter is equipped with a 10 mm  
63 diameter window made of a 50  $\mu m$  thick minimized Mylar film, glued to the detector with a conductive  
64 epoxy. The primary electron clouds resulting from the interaction of x-rays emitted by a  $^{55}Fe$  radioactive  
65 source are multiplied through charge avalanche processes around the anode and the resulting charge is  
66 collected with a charge sensitive pre-amplifier (Canberra 2006). The pre-amplifier signals are fed to a  
67 linear amplifier (Ortec 454), which output is connected to a multichannel analyser.  
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78 The proportional gas used was P10, continuously flowing at a rate of 5 l/h. The gas outlet was  
79 connected, via a reservoir filled with low outgassing oil, to the atmosphere. The inlet and outlet were  
80 equipped with 2  $\mu m$  filters to prevent the  $B_4C$  particles from escaping.  
81  
82

83 The detector was irradiated with 5.9 keV x-rays from a  $^{55}Fe$  source while the anode voltage was varied  
84 from 2000 V to 2400 V. Pulse height distributions were acquired for 60 seconds for each anode voltages,  
85 initially without the microparticles inside the detector and subsequently after depositing 3 grams of  $B_4C$  fine  
86 powder (PlasmaChem GmbH), in the hollow funnel-shaped part of the bottom flange. The method used for  
87 particle dispersion in the gas consisted on violently opening the gas flow for a few seconds and  
88 subsequently reducing it to 8 l/h, the rate used during  
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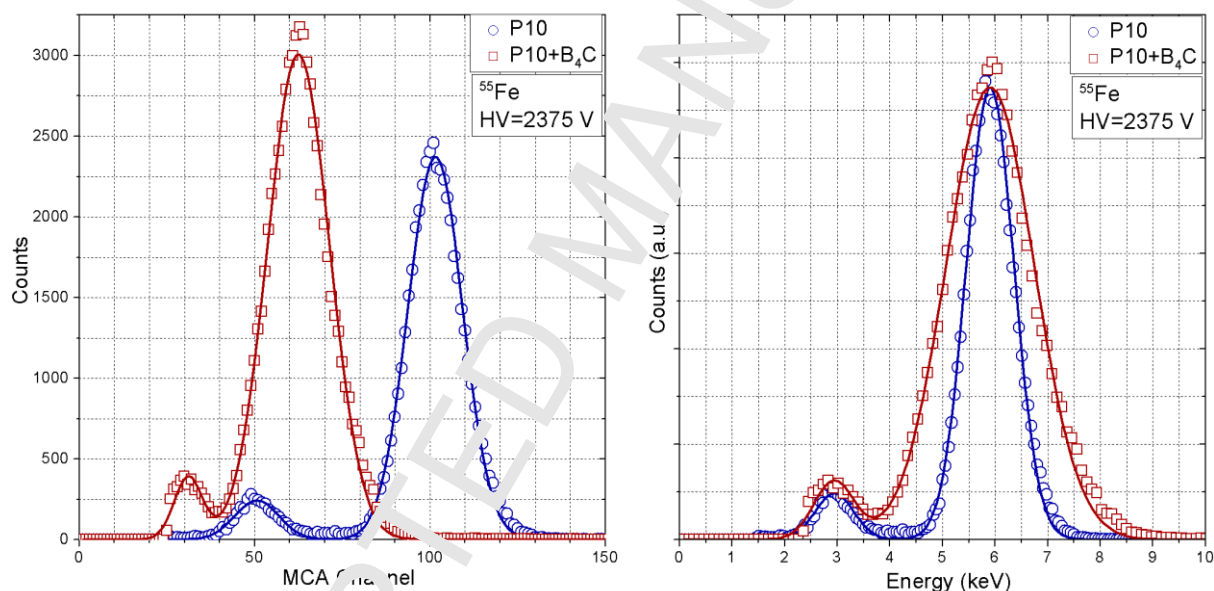
**Fig. 1.** Schematic of the proportional counter used in this work. Differences from [26] are the removal of the field cage copper wires and the addition of a thin Mylar window.

94 data acquisition.

95 A sample of the fine powder used in this work was subject to characterization by laser  
 96 diffraction (Beckman Coulter LS 13 320). Assuming sphere-like particles, the results yield a  
 97 mean diameter value of  $1.056 \mu\text{m}$  ( $d_{10} = 0.553 \mu\text{m}$ ,  $d_{50} = 1.029 \mu\text{m}$  and  $d_{90} = 1.602 \mu\text{m}$ ). It  
 98 should be noticed that the size characterization was performed using ethanol as the suspension  
 99 fluid. Despite the use of rollers, magnetic stirrers and tube rotators to assure the suspension of  
 100 sampled powders, it is impossible to guarantee that the agglomeration behaviour of the  
 101 particles while suspended in liquid ethanol and in gaseous P10 is identical [29]. In addition,  
 102 this behaviour also depends on environmental factors such as temperature and humidity.  
 103 Thus, the  $1.056 \mu\text{m}$  diameter should be considered as nominal value.

### 104 3. Results

105 A comparison of the pulse height distributions recorded for an anode voltage of 2375 V  
 106 without and with  $\text{B}_4\text{C}$  microparticles in the proportional counter is presented in Fig. 2. Along  
 107 with the data points, a double peak Gaussian fit is shown for each pulse height distribution.  
 108 The main peak corresponds to the full absorption of the 5.9 keV x-ray in the proportional gas,  
 109 while the lower amplitude peak corresponds to the  $\text{K}\alpha$  fluorescence escape peak of Ar.



**Fig. 2.** Pulse height distributions recorded with x-rays irradiation from a  $^{55}\text{Fe}$  source and an anode voltage of 2375 V without (blue circles) and with (red squares)  $\text{B}_4\text{C}$  fine powder dispersion. Acquisition time = 60 s. Left: Unnormalized data; Right: Normalization of P10+B $_4\text{C}$  data, to match the counts and centroid of the Gaussian fit taken with just P10.

110 The pulse height distribution is shifted to the lower energy end on the acquisition recorded  
 111 in the presence of the  $\text{B}_4\text{C}$  particles, which was verified throughout all the anode voltage  
 112 range. As shown, the presence of the particles suspended in the gas resulted in a lower charge  
 113 gain achieved by the electron avalanche.

114 In Fig. 2-right, the pulse height distribution taken with the  $\text{B}_4\text{C}$  microparticle aerosol was  
 115 normalized in its vertical and horizontal axes so that its amplitude and centroid match the  
 116 corresponding parameters of the Gaussian fit obtained without the microparticles. The MCA  
 117 (Multichannel analyzer) axis was also calibrated to the energy scale. A broadening of the 5.9  
 118 keV peak after the fine powder dispersion is clearly visible, which implies an energy  
 119 resolution degradation. This effect was observed for the whole range of applied anode  
 120 voltages.

121 Fig. 3 illustrates the gain obtained with  
 122 and without B<sub>4</sub>C microparticles as a  
 123 function of anode voltage. A gain drop by  
 124 a factor of 36%, independent of the anode  
 125 voltage, is observed in the presence of B<sub>4</sub>C  
 126 microparticles. Fig. 3 also suggests that  
 127 this microparticle induced gain drop can  
 128 be compensated by increasing the anode  
 129 voltage by approximately 75 V. A similar  
 130 analysis was performed for the energy  
 131 resolution (*R*). The results, depicted in Fig.  
 132 4, show an average degradation of the  
 133 energy resolution by 15% (absolute value)  
 134 in the presence of B<sub>4</sub>C microparticles, with  
 135 little dependence on the applied anode  
 136 voltage.

137 The intrinsic energy resolution, a  
 138 statistical limit associated with the  
 139 minimum amount of fluctuation that will  
 140 always be present on the detector signal,  
 141 arising from the discrete nature of the  
 142 measured signal itself, was determined for  
 143 each case. Overlooking electronic noise, which is typically a small contributing factor to the  
 144 output signal of proportional counters; intrinsic energy resolution can be derived from [30]:

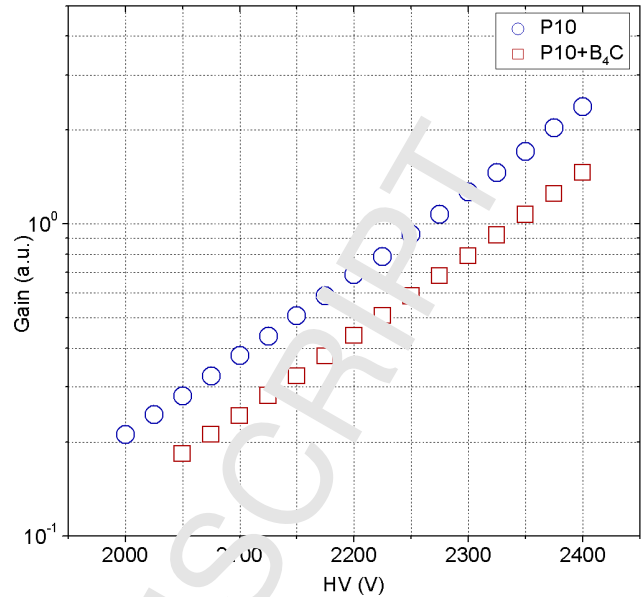
$$145 \quad R = 2.355 \times \sqrt{\frac{(F-1)f}{n_0} + \frac{1}{n_0\bar{G}}} \quad (1)$$

146 where *n*<sub>0</sub> represents the number of primary ion-electron pairs created by the incident  
 147 radiation,  $\bar{G}$  the average gas gain, *F* the Fano factor, *f* the multiplication variance, associated  
 148 to the relative variance of the number of electrons produced in an avalanche assuming a  
 149 Polya distribution and 2.355 the ratio between the full width at half maximum of  
 150 a Gaussian distribution and the standard deviation.

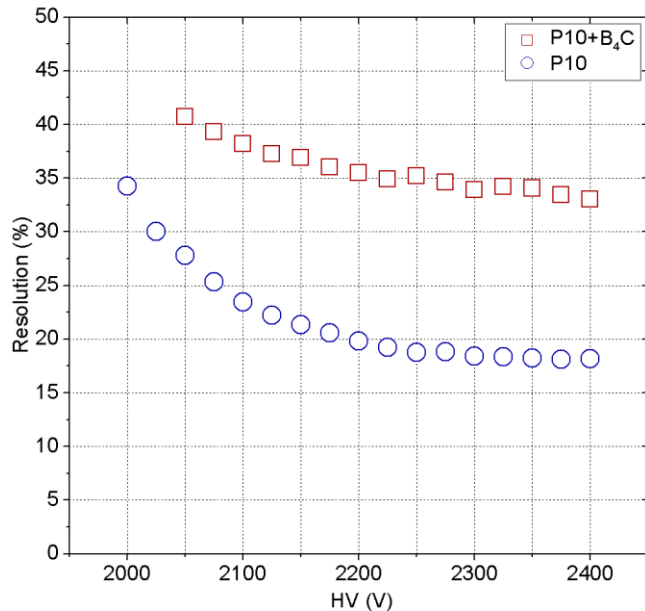
153 The number of primary ion-electron  
 154 pairs produced is proportional to the  
 155 energy deposited by the incident radiation,  
 156 *E<sub>X</sub>*. The proportionality constant between  
 157 them is given by *W*, the mean energy  
 158 required to form one ion-electron pair (26  
 159 eV in argon [30]).

$$160 \quad n_0 = \frac{E_X}{W} \quad (2)$$

161  
 162  
 163 The intrinsic energy resolution can be  
 164 experimentally determined by considering  
 165 the proportionality between the centroids  
 166 of the 5.9 keV peaks in the pulse height  
 167 distributions (*A*) and the detector gain ( $\bar{G}$ ):



**Fig. 3.** Logarithmic plot of the gas gain measured for each anode voltage without (blue circles) and with (red squares) B<sub>4</sub>C fine powder dispersion. An average gain decrease by a factor of 36% was observed.



**Fig. 4** – Energy resolution of the proportional counter versus applied anode voltage without (blue circles) and with (red squares) B<sub>4</sub>C microparticles dispersion. An average energy resolution worsening of 15% (absolute value) was observed when dispersing the B<sub>4</sub>C.

168

$$A \propto n_0 \bar{G} \Rightarrow A = n_0 \bar{G} K_e \quad (3)$$

169 where  $K_e$  is a constant exclusively dependent on the electronics chain detector output. After  
170 the replacements expressed in equations (2) and (3) we can rewrite equation (1) as:

$$171 \quad R = 2.355 \sqrt{\frac{w(F+f)}{E_X} + \frac{K_e}{A}} \Rightarrow R^2 = 5.545 K_e \frac{1}{A} + 5.545 \frac{w(F+f)}{E_X} \quad (4)$$

172 From equation (4), one can see that if, for the same incident energy ( $E_X$ ),  $A$  is varied  
173 throughout a set of acquisitions (accomplished by varying the anode voltage), a linear relation  
174 between  $R^2$  and  $\frac{1}{A}$  is expected. Thus, a plot of  $R^2$  versus  $\frac{1}{A}$  is a reasonable approximation to  
175 extrapolate the intrinsic resolution of the detector, corresponding to value of  $R^2$  when  
176  $(1/A) \rightarrow 0$ , i.e. the y-intercept of the function:

$$177 \quad R_{\text{int}} = 2.355 \sqrt{\frac{w \times (F+f)}{E_X}} \quad (5)$$

178 Since parameters  $w$ ,  $F$  and  $f$  depend  
179 exclusively on the filling gas/aerosol, a  
180 variation of the  $w \times (F + f)$  factor in  
181 the presence of the B<sub>4</sub>C microparticles  
182 is expected and therefore a variation of  
183 the intrinsic energy resolution.

184 Data in Figs. 3 and 4 was processed  
185 according to the method above and the  
186 results are presented in Fig. 5. The  
187 intrinsic energy resolution ( $R_{\text{int}}$ )  
188 obtained when the detector was filled  
189 with P10 gas was of 15%, increasing  
190 with the microparticles dispersion to  
191 32%. Only the linear region of each  $R^2$   
192 versus  $\frac{1}{A}$  curve, limited by the vertical  
193 dashed lines in Fig. 5, was considered  
194 for fitting. This was because the  
195 effects that cause loss of linearity are  
196 not contemplated in equation (4),  
197 namely fluctuations in the number of  
198 primary electrons reaching the  
199 avalanche region for low voltages and  
200 fluctuations in the electric field due to the spatial positive charge accumulated for high  
201 voltages.

202 As expected, the linear portions of the curves are almost parallel, since the slope  
203 determined by  $K_e$  is similar for both cases.

204

#### 205 4. Discussion

206 One significant concern regarding this detection concept was that dispersing fine powder  
207 in a proportional counter could lead to the occurrence of electrical discharges, compromising  
208 its operation. In effect, B<sub>4</sub>C fine powder was selected in [26] not only for the presence of the

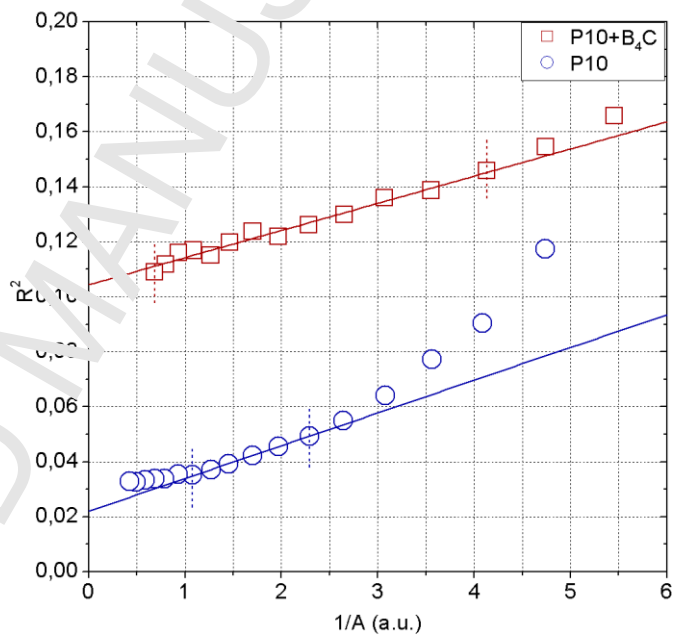


Fig. 5. Square of the energy resolution versus  $1/A$  without (blue circles) and with (red squares) B<sub>4</sub>C fine powder dispersion. The extrapolated intrinsic energy resolution values are 15% and 32%, respectively.

209 neutron sensitive  $^{10}\text{B}$  isotope, but also due to its insulating properties. In this work, the  
 210 presence of the fine powder did not severely affect the proportional counter by causing  
 211 discharges or other electrical instabilities during acquisition using soft x-rays.

212 The microparticles affected however the proportional counter performance, influencing  
 213 the achievable charge gain and energy resolution. Despite the observed charge gain reduction,  
 214 the 5.9 keV peak still exhibits a symmetric Gaussian shape (Fig. 2). This indicates that the  
 215 gain drop is not due to electrons of the avalanches being captured by microparticles. If that  
 216 were the case, a tail at lower energies would be present on the pulse height distribution as the  
 217 number of captured electrons would depend on the path travelled.

218 An analysis of the intrinsic resolution without and with microparticle dispersion provides  
 219 an insight on the reasons behind the degradation of these parameters. From equation (5) we  
 220 conclude the factor  $w \times (F + f)$  has increased by a factor of 4.8 with the inclusion of the  
 221 microparticles:

$$222 \frac{w_{aerosol} \times (F+f)_{aerosol}}{w_{P10} \times (F+f)_{P10}} = 4.8 \quad (6)$$

223  
 224 An increase in  $w$  due to the inclusion of microparticles is excluded by a pulse height  
 225 distribution analysis. The discrete nature of the microparticles would cause any process  
 226 induced by their presence to be also of non-continuous nature, affecting each event according  
 227 to its degree of interaction with the microparticle. This would create changes in the pulse  
 228 height distributions, most notably a tail for low energies on the 5.9 keV peak and an increase  
 229 of the escape peak relative amplitude, which were not present in Fig. 2.

230 Therefore, we conclude that the increase in the  $w \times (F + f)$  factor is due to an increase in  
 231 the avalanche gain fluctuations ( $F + f$ ), consequence of the electric field distortion in the  
 232 region near the microparticle, depending on particle shape and relative orientation to the  
 233 electric field.

## 234 5. Conclusions

235 The operation of a proportional counter with neutron sensitive  $\text{B}_4\text{C}$  microparticles  
 236 suspended in P10 gas was studied by irradiation with soft x-rays (5.9 keV). We compared the  
 237 detector gain, energy resolution and intrinsic energy resolution with and without the  
 238 dispersion of  $\text{B}_4\text{C}$  microparticles: a gain decrease by a factor of 36% and an energy resolution  
 239 increase by 15% (absolute value) are observed. Intrinsic energy resolution worsens by  
 240 approximately 17% (absolute value) in the presence of microparticles.

241 The degradation of these parameters is justified by the increment of the  $w \times (F + f)$   
 242 factor, which indicates a rise on the fluctuations in the avalanche charge gain, associated with  
 243 ( $F + f$ ), due to inhomogeneities in the electric field created by the microparticles.

244 It is important to notice that the fine powder did not compromise the detector operation by  
 245 causing electrical discharges or drastically affecting its charge gain.

246 This work contributes to the validation of the fine powder aerosol as a radiation detection  
 247 medium in proportional counters. The detection technique can, in principle, also be used to  
 248 increase detection efficiency of gaseous detectors to distinct radiation sources. For instance,  
 249 we can infer that detection of hard x-rays and gamma-rays based on this concept is possible  
 250 using adequate micro/nanoparticles, made of high  $Z$  number materials, such as Bi or Au.  
 251 While an increase in detection efficiency is expected, it would not come without  
 252 compromising the achievable gain and energy resolution. The former can be compensated by  
 253 increasing the electric field, while the later cannot.



254 Ultimately, the discussed technique is an interesting solution for applications in which  
 255 detection efficiency is favored over energy resolution. Further tests focusing on hard x-  
 256 rays/gamma-rays irradiation must be carried to validate of the practicability of this detection  
 257 technique for application in this energy range. In addition, the buildup of deposits or the  
 258 development of micro/nanoparticles induced corrosion of the mechanical components will  
 259 also be evaluated by means of microscope and SEM images of the anode wire, cathode wall  
 260 and insulator elements, as a function of detector operation time.  
 261

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 267 Internationalization, COMPETE 2020.

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