

Supplementary Materials

First Stage of the Development of an Eco-Friendly Detergent Formulation for Efficient Removal of Carbonized Soil

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In this work, the commercial degreaser KH7, from KH Lloreda company, was used. This degreaser is composed of water, fatty ethoxylated alcohol, methoxypropanol, monoethanolamine and polycarboxylate with a pH of 11.25.

Tables

Table S1. pH of the different formulations used in the screening.

Surfactant ↓	Solvent →	pH			
		PM	DPM	BDG	MMB
[N ₁₁₁₈][C ₈ O ₂]		10.36	7.91	8.53	8.54
[N ₁₁₁₈][C ₁₀ O ₂]		8.87	8.20	8.28	8.28
[N ₁₁₁₈][C ₁₂ O ₂]		9.02	8.48	9.06	8.84
[N ₁₁₁₁₀][C ₈ O ₂]		10.19	8.32	9.82	7.86
[N ₁₁₁₁₀][C ₁₀ O ₂]		9.21	8.45	8.83	8.83
[N ₁₁₁₁₀][C ₁₂ O ₂]		9.30	8.56	8.33	8.10
[N ₁₁₁₁₂][C ₁₀ O ₂]		9.35	8.39	8.75	9.15
[N ₁₁₁₁₂][C ₁₂ O ₂]		9.65	8.62	9.00	9.30
C ₁₂ -C ₁₅ 7EO's		5.08	4.15	4.99	4.05
C ₁₀ 6EO's		4.68	4.04	4.67	3.18
C ₁₂ -C ₁₅ 9EO's		5.80	4.30	5.94	4.19
C ₁₁ -C ₁₃ 9EO's		5.07	3.95	4.99	3.90
C ₁₀ -C ₁₄ 8EO's		5.10	4.05	4.86	3.98

Table S2. *HLB* values of nonionic surfactants, given by the suppliers.

Nonionic surfactant	HLB
C ₁₀ 6EO's	12.4
C ₁₁ -C ₁₃ 9EO's	13.2
C ₁₂ -C ₁₅ 7EO's	12.3
C ₁₂ -C ₁₅ 9EO's	13.1
C ₁₀ -C ₁₄ 8EO's	13.6

Table S3. Mixture design for optimization of the solvent composition.

Run	Coded variables		
	Surfactant (wt%)	Solvent (wt%)	Water (wt%)
1	10.00	13.00	77.00
2	10.00	3.00	87.00
3	3.00	13.00	84.00
4	3.00	3.00	94.00
5	3.00	8.00	89.00
6	10.00	8.00	82.00
7	6.50	3.00	90.50
8	6.50	13.00	80.50
9	6.50	8.00	85.50

Table S4. pH and efficiency obtained for the formulations used in the mixture design of C₁₁-C₁₃9EO's, IPG and water.

Model for ceramic: $R^2 = 0.97$ and $R^2_{adj.} = 0.91$

Model for stainless-steel: $R^2 = 0.80$ and $R^2_{adj.} = 0.47$

Run	pH	Experimental Efficiency		Predicted Efficiency	
		Ceramic	Stainless-steel	Ceramic	Stainless-steel
1	4.24	0.45	0.65	0.42	0.61
2	4.09	0.76	0.87	0.79	0.80
3	4.24	1.02	0.87	0.99	0.93
4	4.18	0.60	0.90	0.62	0.92
5	4.19	0.90	0.90	0.90	0.83
6	4.15	0.70	0.51	0.70	0.61
7	4.30	0.93	0.82	0.87	0.86
8	4.20	0.82	0.80	0.87	0.78
9	4.14	0.96	0.74	0.97	0.72

Table S5. pH and efficiency obtained for the formulations used in the mixture design of $[N_{1118}][C_8O_2]$, BDG and water.

Model for ceramic: $R^2 = 0.94$ and $R^2_{adj.} = 0.84$

Model for stainless-steel: $R^2 = 0.92$ and $R^2_{adj.} = 0.80$

Run	pH	Experimental Efficiency		Predicted Efficiency	
		Ceramic	Stainless-steel	Ceramic	Stainless-steel
1	8.23	0.87	1.10	0.83	1.06
2	8.74	0.63	0.95	0.65	0.93
3	7.58	0.47	1.03	0.41	0.99
4	7.92	0.32	0.41	0.31	0.40
5	7.70	0.25	0.65	0.33	0.70
6	8.41	0.68	0.93	0.70	0.99
7	7.83	0.87	0.68	0.87	0.71
8	8.05	0.90	0.98	1.00	1.06
9	8.15	1.00	1.00	0.90	0.89

Table S6. ANOVA for the mixture design using formulations composed of C₁₁-C₁₃ 9EOs, IPG and water applied to the ceramic surface.

	SS	df	MS	F	p
Model (Regression)	0.265929	5	0.053186	17.30503	0.020203
Total Error (Residual)	0.009220	3	0.003073		
Total Adjusted	0.275149	8	0.034394		

Table S7. ANOVA for the mixture design using formulations composed of C₁₁-C₁₃ 9EOs, IPG and water applied to the stainless-steel surface.

	SS	df	MS	F	p
Model (Regression)	0.110659	5	0.022132	3.399777	0.051053
Total Error (Residual)	0.027667	3	0.009222		
Total Adjusted	0.138327	8	0.017291		

Table S8. Efficiency and pH obtained for the optimal composition of the formulation composed of C₁₁-C₁₃9EO's, IPG and water.

Surface	Optimal composition			Efficiency		Relative deviation (%)	pH
	IPG	C ₁₁ -C ₁₃ 9EO's	H ₂ O	Experimental	Predicted		
Ceramic	10.0	5.0	85.0	1.03	1.00	3.00	4.30
Stainless-steel	13.0	3.0	84.0	0.95	0.91	4.40	4.24

Table S9. ANOVA for the mixture design using formulations composed of [N₁₁₁₈][C₈O₂], BDG and water applied to the ceramic surface.

	SS	df	MS	F	p
Model (Regression)	0.54402678	5	0.108805	9.313672	0.04783
Total Error (Residual)	0.03504698	3	0.011682		
Total Adjusted	0.57907375	8	0.072384		

Table S10. ANOVA for the mixture design using formulations composed of $[N_{1118}][C_8O_2]$, BDG and water applied to the stainless-steel surface.

	SS	df	MS	F	p
Model (Regression)	0.381089	5	0.076218	7.227412	0.047155
Total Error (Residual)	0.031637	3	0.010546		
Total Adjusted	0.412726	8	0.051591		

Table S11. Efficiency and pH obtained for the optimal composition of the formulation composed of $[N_{1118}][C_8O_2]$, BDG and water.

Surface	Optimal composition			Efficiency		Relative deviation (%)	pH
	BDG	$[N_{1118}][C_8O_2]$	H_2O	Experimental	Predicted		
Ceramic	13.0	7.0	80.0	0.99	1.03	3.90	8.28
Stainless-steel	13.0	8.0	79.0	1.04	1.07	2.80	8.63

Figures

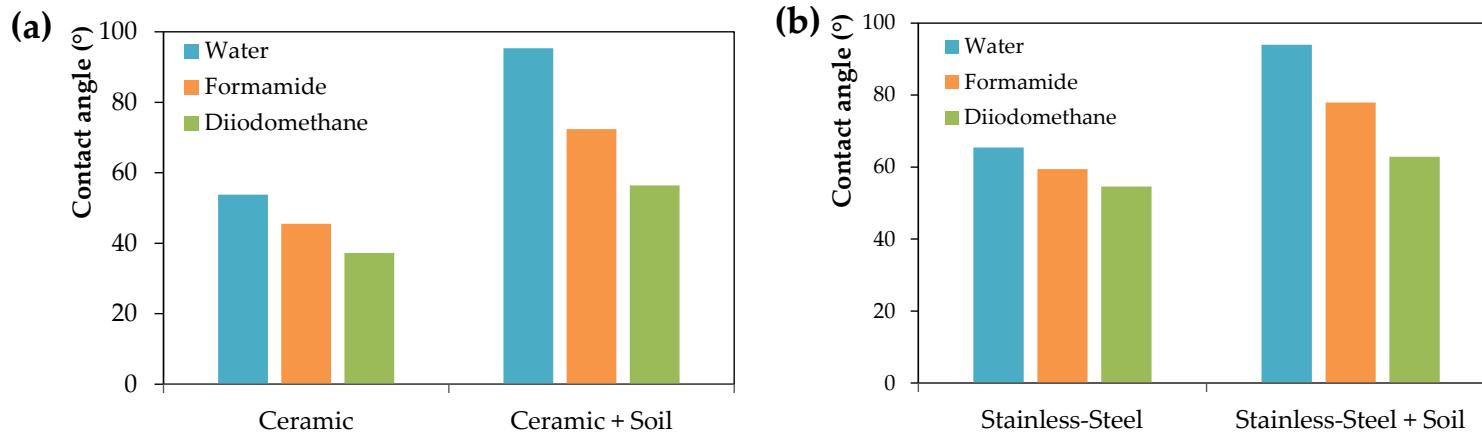


Figure S1. Contact angles of net and soiled surfaces: (a) ceramic and (b) stainless-steel.

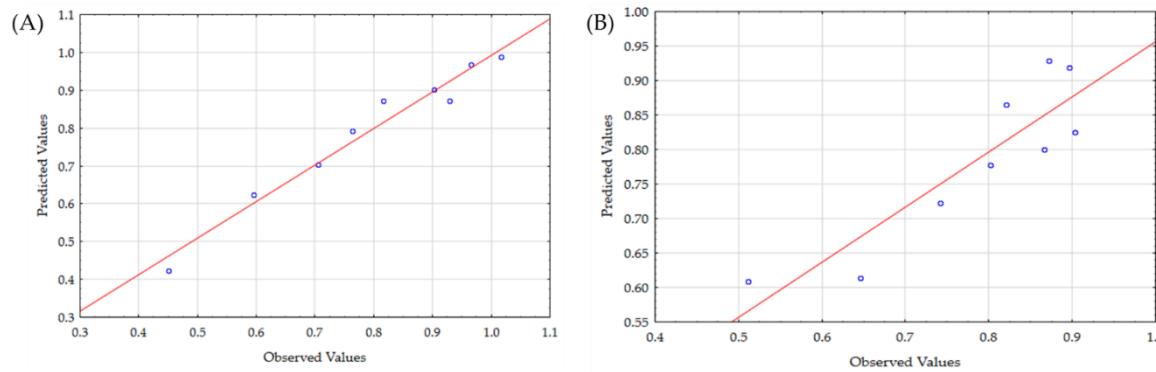


Figure S2. Predict vs. observed values of IPG + C₁₁-C₁₃ 9EO's for soil's removal from (A) ceramic and (B) stainless-steel.

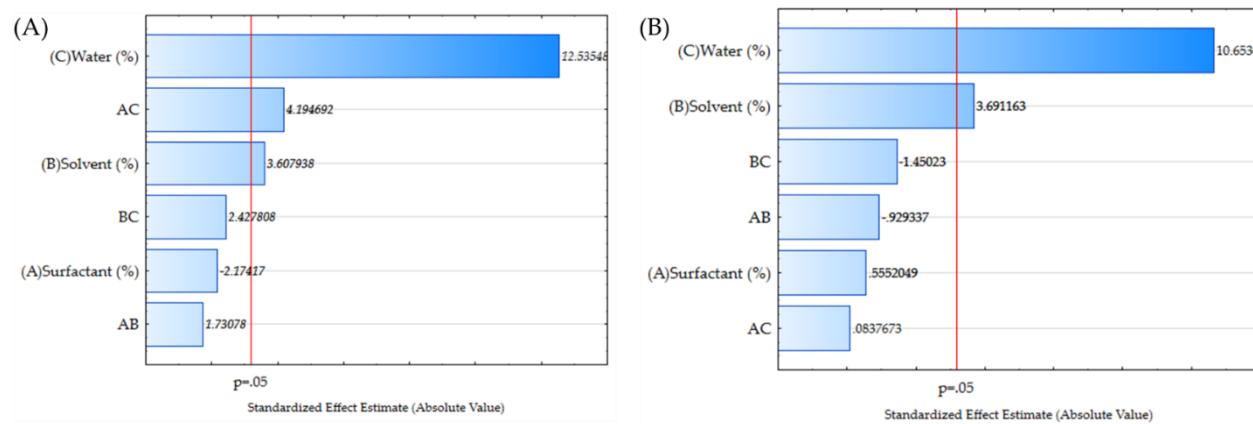


Figure S3. Pareto charts for the standardized main effects in the IPG + C₁₁-C₁₃ 9EO's mixture design for (A) ceramic and (B) stainless-steel. The vertical line indicates the statistical significance of the effects (95% of confidence).

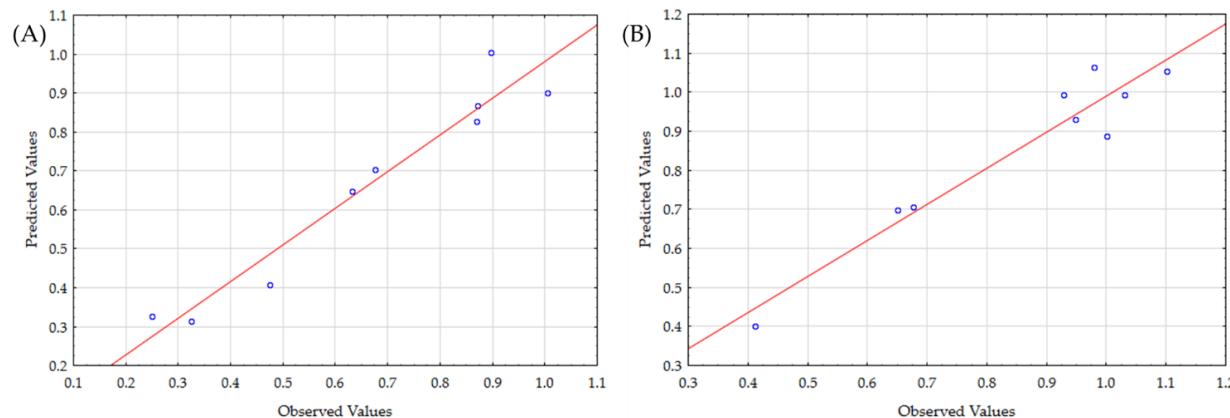


Figure S4. Predict vs. observed values of BDG + [N₁₁₁₈][C₈O₂] for soil's removal from (A) ceramic and (B) stainless-steel.

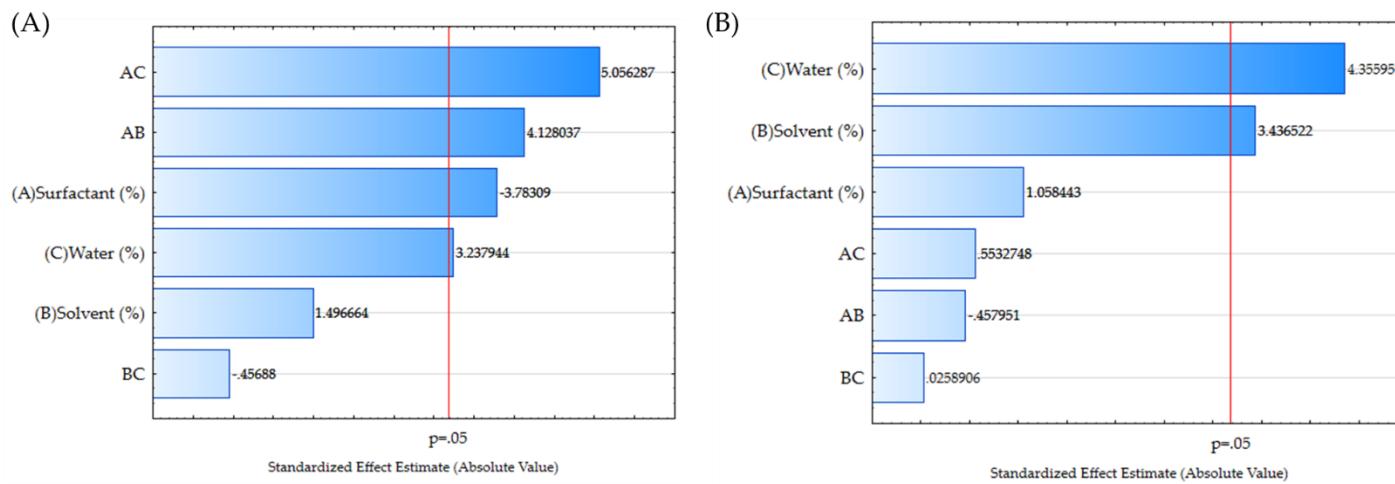
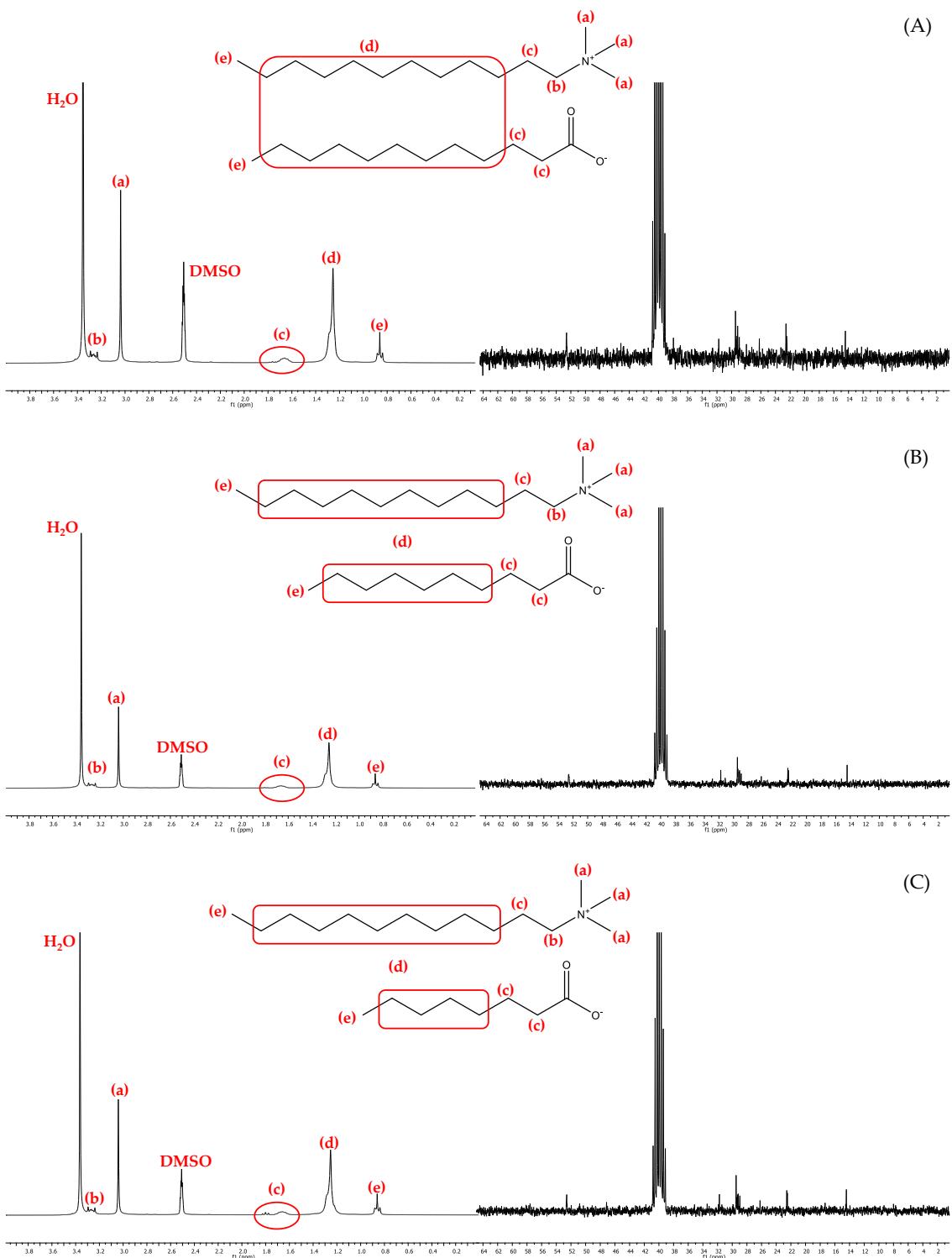
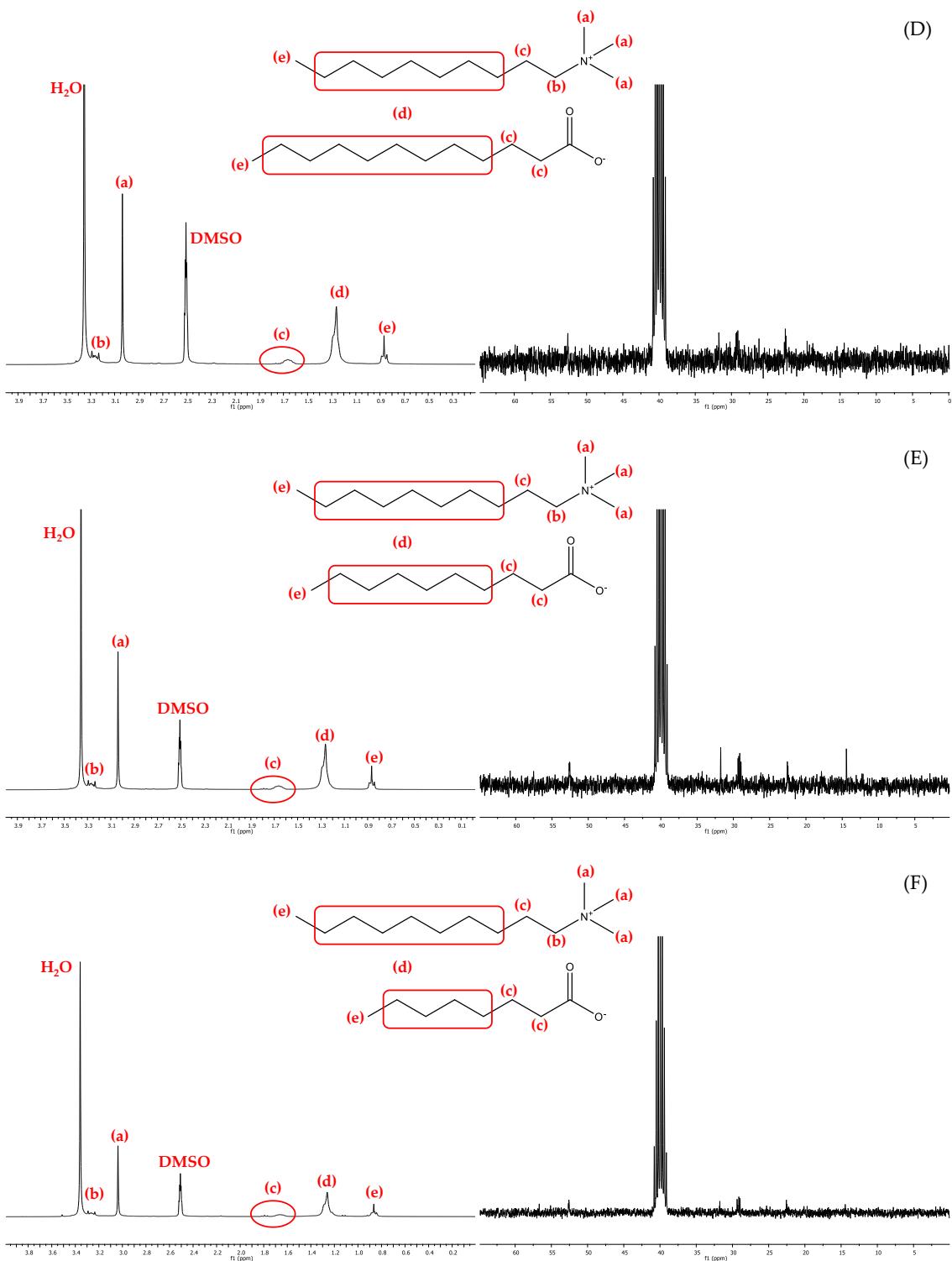


Figure S5. Pareto charts for the standardized main effects in the BDG + [N₁₁₁₈][C₈O₂] mixture design for (A) ceramic and (B) stainless-steel. The vertical line indicates the statistical significance of the effects (95% of confidence).





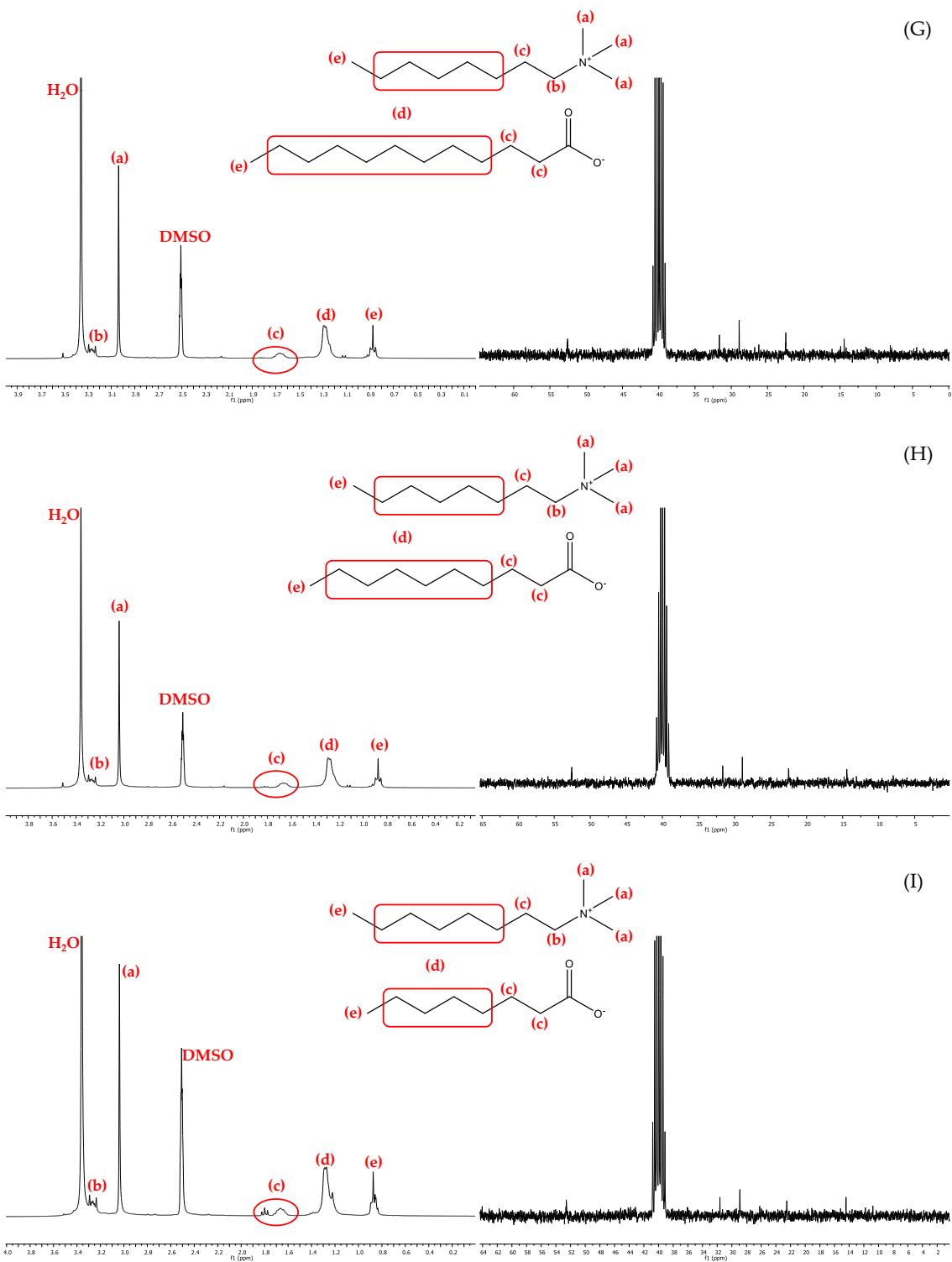


Figure S6. ^1H (left panel) and ^{13}C (right panel) NMR spectra in DMSO of the ionic surfactants synthesized: (A) $[\text{N}_{11112}][\text{C}_{12}\text{O}_2]$; (B) $[\text{N}_{11112}][\text{C}_{10}\text{O}_2]$; (C) $[\text{N}_{11112}][\text{C}_8\text{O}_2]$; (D) $[\text{N}_{11110}][\text{C}_{12}\text{O}_2]$; (E) $[\text{N}_{11110}][\text{C}_{10}\text{O}_2]$; (F) $[\text{N}_{11110}][\text{C}_8\text{O}_2]$; (G) $[\text{N}_{1118}][\text{C}_{12}\text{O}_2]$; (H) $[\text{N}_{1118}][\text{C}_{10}\text{O}_2]$; (I) $[\text{N}_{1118}][\text{C}_8\text{O}_2]$.